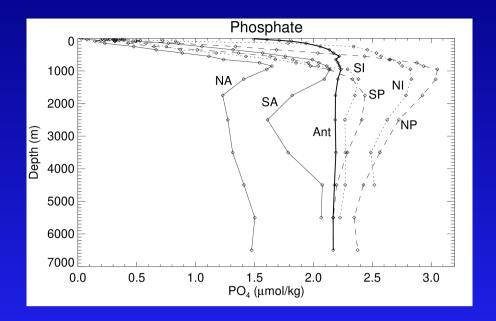
# THE OCEAN CARBON CYCLE

#### 21st February 2024

- 1 Box-model of the global ocean phosphorus, alkalinity, carbon
- 2 Pre-industrial model
- 3 Evolution during the industrial period
- 4 <sup>13</sup>C isotopic evolution

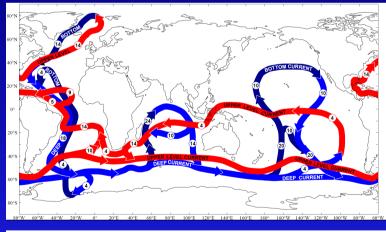
BOX-MODEL OF THE GLOBAL OCEAN Phosphorus, Alkalinity, Carbon

#### PHOSPHATE DISTRIBUTION IN THE OCEAN

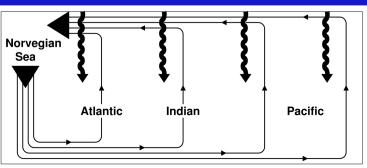


Ant – Antarctic; •A – Atlantic; •I – Indian; •P – Pacific; N• and S• – Northern and Southern parts of •, resp.

#### THERMOHALINE CIRCULATION

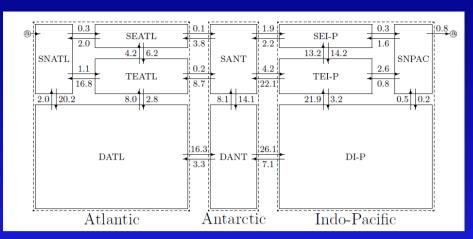


surface-todeep-sea gradient



inter-basin gradient

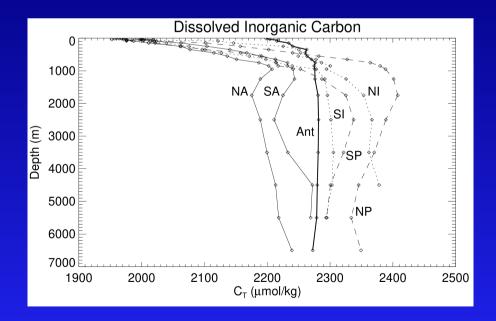
#### **MODEL STRUCTURE**



Water fluxes in Sverdrup (Sv): 1 Sv = 10<sup>6</sup> m<sup>3</sup> s<sup>-1</sup>

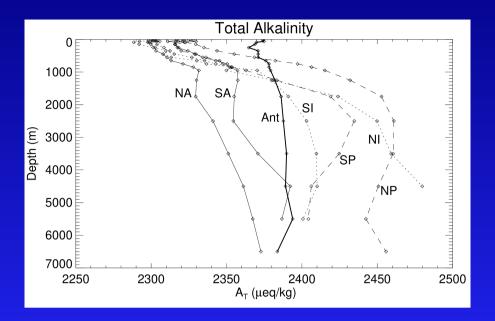
E	Basin	Input flux (m3/yr)	Output flux (m3/yr)	Reservoir budget (m3/yr)	Turnover Time (yr)
1 5	SNATL	0.68117760E+15	0.68117760E+15	0.0000000E+00	17.62
2 5	SEATL	0.26174880E+15	0.26174880E+15	0.0000000E+00	22.92
3 5	SANT	0.10312272E+16	0.10312272E+16	0.0000000E+00	70.79
4 5	SEI-P	0.52665120E+15	0.52665120E+15	0.0000000E+00	34.18
5 5	SNPAC	0.10722240E+15	0.10722240E+15	0.0000000E+00	121.24
6 1	<b>TEATL</b>	0.75686400E+15	0.75686400E+15	0.0000000E+00	72.67
7 1	TEI-P	0.12961296E+16	0.12961296E+16	0.0000000E+00	120.36
8 [	DATL	0.82939680E+15	0.82939680E+15	0.0000000E+00	245.96
9 [	DANT	0.11826000E+16	0.11826000E+16	0.0000000E+00	184.34
10 [	DI-P	0.93031200E+15	0.93031200E+15	0.0000000E+00	628.82

#### **DIC DISTRIBUTION IN THE OCEAN**



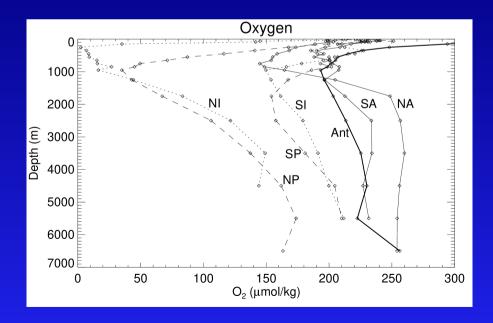
Ant – Antarctic; •A – Atlantic; •I – Indian; •P – Pacific; N• and S• – Northern and Southern parts of •, resp.

#### **ALKALINITY DISTRIBUTION IN THE OCEAN**



Ant – Antarctic; •A – Atlantic; •I – Indian; •P – Pacific; N• and S• – Northern and Southern parts of •, resp.

#### **OXYGEN DISTRIBUTION IN THE OCEAN**

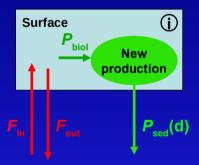


Ant – Antarctic; •A – Atlantic; •I – Indian; •P – Pacific; N• and S• – Northern and Southern parts of •, resp.

### PRE-INDUSTRIAL MODEL

#### PHOSPHORUS: PRODUCTIVITY CONTROL

#### **Surface boxes**



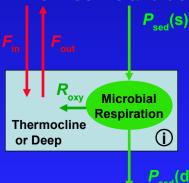
#### **Input Fluxes:**

$$F_{in} = \sum_{j} w_{jj} c_{j}$$
 (advection) with  $c_{j} = Q_{j}/V_{j}$ 

#### **Output Fluxes:**

$$F_{\text{out}} = (\sum_{j} W_{ij}) c_{ij}$$
 (advection)  
 $P_{\text{sed}}(d) = P_{\text{biol}} = \Phi_{\text{ut}} \cdot F_{\text{in}}$  (new production)  
 $\rightarrow \Phi_{\text{ut}}$  lower at high latitudes

#### Thermocline and deep boxes



#### **Input Fluxes:**

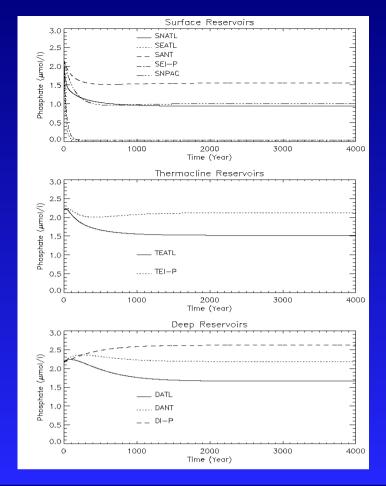
$$F_{in} = \sum_{j} w_{ji} c_{j}$$
 (advection)  
 $R_{oxy} = k_{oxy} \cdot P_{sed}(s)$  (microbial respiration)  
 $P_{sed}(d) = P_{sed}(s) \cdot R_{oxy}$ 

#### **Output Fluxes:**

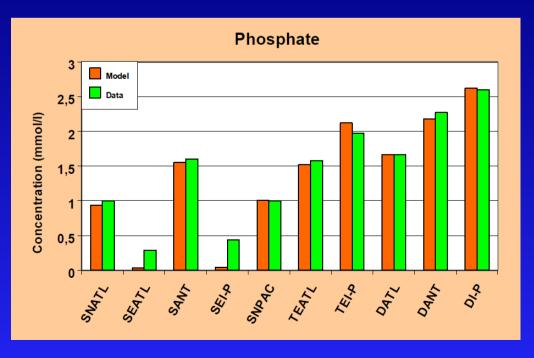
$$F_{\text{out}} = (\sum_{i} w_{ij}) c_{i}$$
 (advection)

#### PRE-INDUSTRIAL STEADY-STATE SOLUTION (PHOSPHORUS)

- → Integration: 4000 years
- → Initial conditions: Homogeneous ocean (c = 2.164 µmol P/litre)



#### **COMPARISON WITH DATA: PHOSPHORUS**



Data: Geosecs ('70)

#### **CARBON AND ALKALINITY**

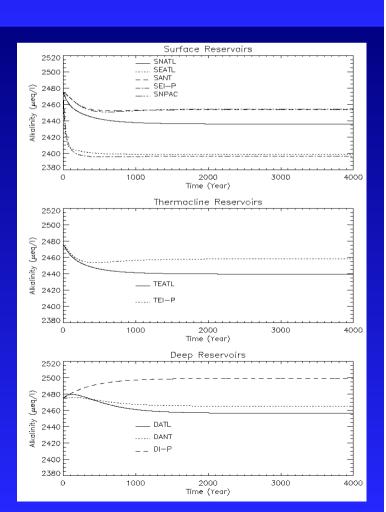
- Model linked to the phosphorus model through the usage elemental ratios
- At the surface: C<sub>org</sub> and CaCO<sub>3</sub> (aragonite/calcite) production
  - $\rightarrow$  C<sub>org</sub>: C/P = 106/1 (Redfield)
  - $\rightarrow$  CaCO<sub>3</sub>:  $r_{carb}$  = CaCO<sub>3</sub>/C<sub>org</sub> (adjustable parameter)
- In the thermocline: partial oxidation of  $C_{org} (\rightarrow k_{oxy})$ 
  - → C/P = 106/1 (Redfield)
- At depth:
  - $\rightarrow$  oxidation of the remaining  $C_{\text{org}} (\rightarrow 1-k_{\text{oxy}})$
  - → dissolution of CaCO<sub>3</sub>
- In each box: pH calculation and carbonate speciation
- Exchange with the atmosphere in each surface reservoir i:

$$\rightarrow F_{a0} = k_{a0}$$
. area(i). (pCO<sub>2</sub> - pCO<sub>2</sub>(i))

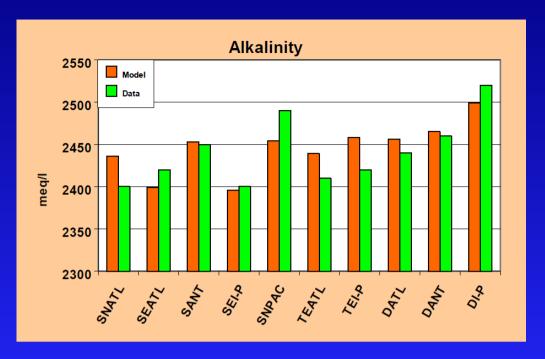
# PRE-INDUSTRIAL STEADY-STATE SOLUTION (ALKALINITY)

- → integration: 4000 years
- → initial conditions: homogeneous ocean (Alk = 2474 µeq/litre)

$$\rightarrow$$
  $r_{carb} = CaCO_3/C_{org}$ 

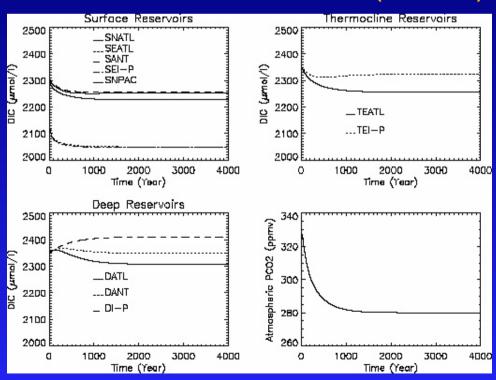


#### **COMPARISON WITH DATA: ALKALINITY**



Data: Geosecs ('70)

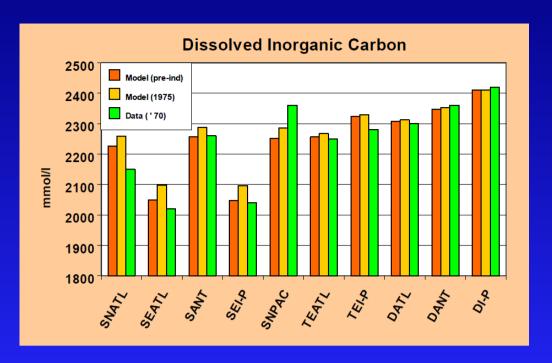
#### PRE-INDUSTRIAL STEADY STATE (CARBON)



**Initial conditions:** 

Homogeneous ocean (DIC = 2350 μmol/I), pCO<sub>2</sub>(atm) = 280 ppmv

#### **COMPARISON WITH DATA: CARBON**

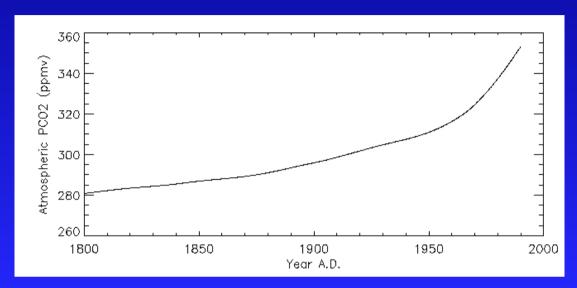


Data: Geosecs ('70)

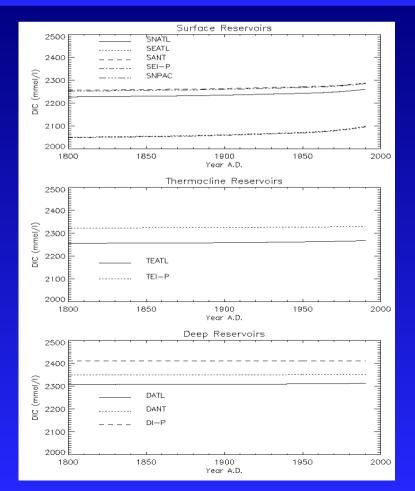
## EVOLUTION DURING THE INDUSTRIAL PERIOD

## FORCING OF THE MODEL FOR THE INDUSTRIAL PERIOD

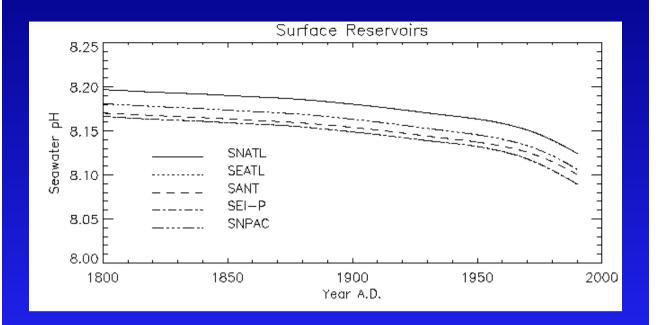
- → Initial conditions in 1800 provided by the previously calculated pre-industrial steady state
- → Evolution of atmospheric CO<sub>2</sub> prescribed from 1800 to 1990



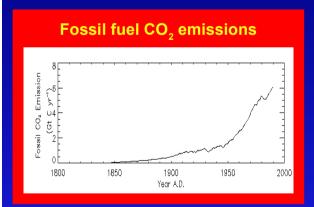
EVOLUTION OF DISSOLVED INORGANIC CARBON



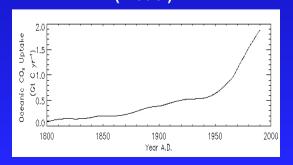
#### **EVOLUTION OF PH IN THE SURFACE RESERVOIRS**



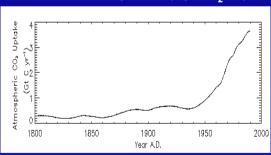
## FLUX BALANCE OF ATMOSPHERIC CO<sub>2</sub> FOR THE INDUSTRIAL PERIOD



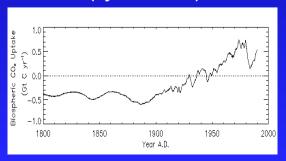
## Transfer to the ocean (model)



## Rate of change in the atmosphere (dpCO<sub>2</sub>/dt)



## Transfer to the biosphere (by difference)



## ATMOSPHERIC CO<sub>2</sub> BALANCE (1980-1990) (Gt C yr<sup>-1</sup>)

#### **SOURCES**

Fossil fuels & cements Land-use change	This work 5.44 1.57	IPCC 1995 5.5 ± 0.5 1.6 ± 1.0
Total	7.01	7.1 ± 1.0
SINKS		
Atmosphere Ocean (Model)	3.40 1.71	3.3 ± 0.2 2.0 ± 0.8
Difference (→ terrestrial biosphere)	1.90	1.8 ± 1.5

13C ISOTOPIC EVOLUTION

#### **CARBON ISOTOPES**

Three naturally occuring carbon isotopes:

<sup>12</sup>C ~ 98.94 ± 0.10%

 $^{13}$ C ~ 1.06 ± 0.10%

<sup>14</sup>C (radiogenic, radioactive) trace amounts

#### where:

 $C_i$  = carbon content of reservoir i

 $F_{ii}$  = flux entering reservoir i (from reservoir j)

 $F_{ii}$  = flux leaving reservoir i (for reservoir j)

 $\delta_i = \delta^{13}$ C of the carbon in reservoir *i* 

 $\delta_{ii} = \delta^{13}$ C of flux  $F_{ii}$  (into reservoir i)

 $\delta_{ij} = \delta^{13}$ C of flux  $F_{ij}$  (out of reservoir i)

Notice: output fluxes only have to be considered if they are subject to fractionation, i. e., if  $\Delta = \delta_{ii} - \delta_i \neq 0$ 

#### ISOTOPIC EVOLUTION EQUATION

The equation describing the evolution of the isotopic composition of a reservoir *i* in time can be written (approximation):

$$d\delta_{i} / dt = \left[ \sum_{j \neq i}^{j} F_{ij} \left( \delta_{ji} - \delta_{i} \right) - \sum_{j \neq i}^{j} F_{ij} \left( \delta_{ij} - \delta_{i} \right) \right] / C_{i}$$

#### where:

 $C_i$  = carbon content of reservoir i

 $F_{ii}$  = flux entering reservoir i (from reservoir j)

 $\vec{F}_{ii}$  = flux leaving reservoir *i* (for reservoir *j*)

 $\delta_i = \delta^{13}$ C of the carbon in reservoir *i* 

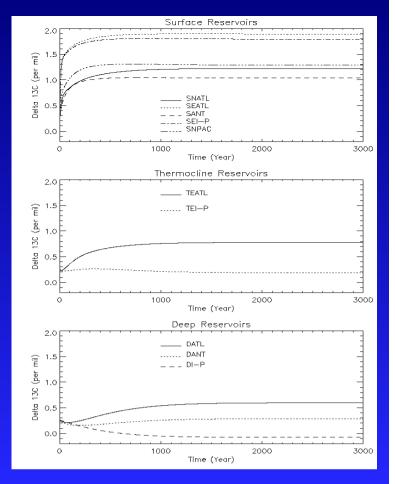
 $\delta_{ii} = \delta^{13}$ C of flux  $F_{ii}$  (into reservoir i)

 $\delta_{ii} = \delta^{13}$ C of flux  $F_{ii}$  (out of reservoir i)

Notice: output fluxes only have to be considered if they are subject to fractionation, i. e., if  $\Delta = \delta_{ii} - \delta_i \neq 0$ 

# PRE-INDUSTRIAL STEADY-STATE SOLUTION $(\delta^{13}C)$

- → integration: 3000 years
- → initial conditions: homogeneous ocean (δ¹³C = 0.259 ‰)



## EVOLUTION OF $\delta^{13}$ C DURING THE INDUSTRIAL PERIOD (coupled ocean-atmosphere-biosphere model)

